

AQUIFER TEST  
MARTIN WELLS, OKANOGAN COUNTY, WASHINGTON

At the request of personnel of the Central Region, an aquifer test was conducted on October 11, 12, 13, 1977 near Omak in Okanogan County.

The primary purpose of the test was to determine possible hydraulic continuity between the wells, and aquifer constants.

Three wells were used in the test. The pumped well (RM #2) belongs to Mr. R. Martin and is located in 34/26E-2C2. The two wells which were used for observational purposes are owned by Mr. D. Martin and are 34/26E-2B2 (DM #2) which is 169 feet ESE of the pumped well and 34/26E-2B1 (DM #1) which is 31 feet east of DM#2 and 200 feet ESE of RM#2 (Figure 1).

The wells are developed in an unconfined aquifer of Quaternary age consisting of clasts ranging in size from silt to boulders which were deposited by glacial melt water streams. Outcrops of bedrock throughout the immediate area constitute impermeable boundary conditions which complicate the interpretation of the test data. No significant pumping had taken place for several days before the test and the aquifer was assumed to be essentially in a nonstressed condition.

The electric turbine pump was started at 1140 hrs. on October 11, 1977 and a pumping rate (Q) of 508 gallons per minute (gpm) was quickly established and maintained. Q, determined by timing the filling of a 55 gallon container, was checked repeatedly throughout the 24 hour pumping test. Drawdown measurements were made in all three wells; however, because of difficulties encountered

in getting reliable readings none were taken in the pumped well during the last 18 hours of pumping.

After 24 hours, the water levels in DM#2 and DM#1 had dropped 3.05 feet and 2.63 feet respectively. The pump was shut off and recovery was measured. After 10 hours, wells DM#2 and DM#1 had recovered to within 1.40 ft. and 1.44 ft., respectively, of the static water levels measured at the beginning of the test. The pumped well (RM#2) had recovered to within 1.33 ft. of the prepumping level. Copies of all data are attached.

The drawdown data for the observation well DM#2 were plotted on logarithmic graph paper (Fig. 2) and using the curve corresponding to the latter part of the test and the Theis type curve, a transmissivity (T) of  $2.9 \times 10^4$  gallons per day per foot (gpd/ft) and a storage coefficient (S) of .07 were determined.

Using the following formulae and constants, one can investigate withdrawal/drawdown possibilities. It is stressed that the calculated figures are probably conservative because of the likelihood of additional impermeable boundaries.

$$U = \frac{1.87 \times r^2 \times S}{T \times t \text{ days}} \quad s = \frac{114.6 \times Q \times W_u}{T}$$

$T = 2.9 \times 10^4$  gpd/ft                       $S = .07$   
 $r = 169$  ft (distance from RM#1 to DM#2)

A groundwater certificate for 600 gpm and 400 AF/yr for the irrigation of 100 acres from RM#1 has been issued. Of the 100 acres, 80 acres is for land belonging to Ralph Martin and 20 acres is for land owned by Dean Martin.

If the place of withdrawal for the irrigation of 20 acres were changed to DM#2, the following would apply:

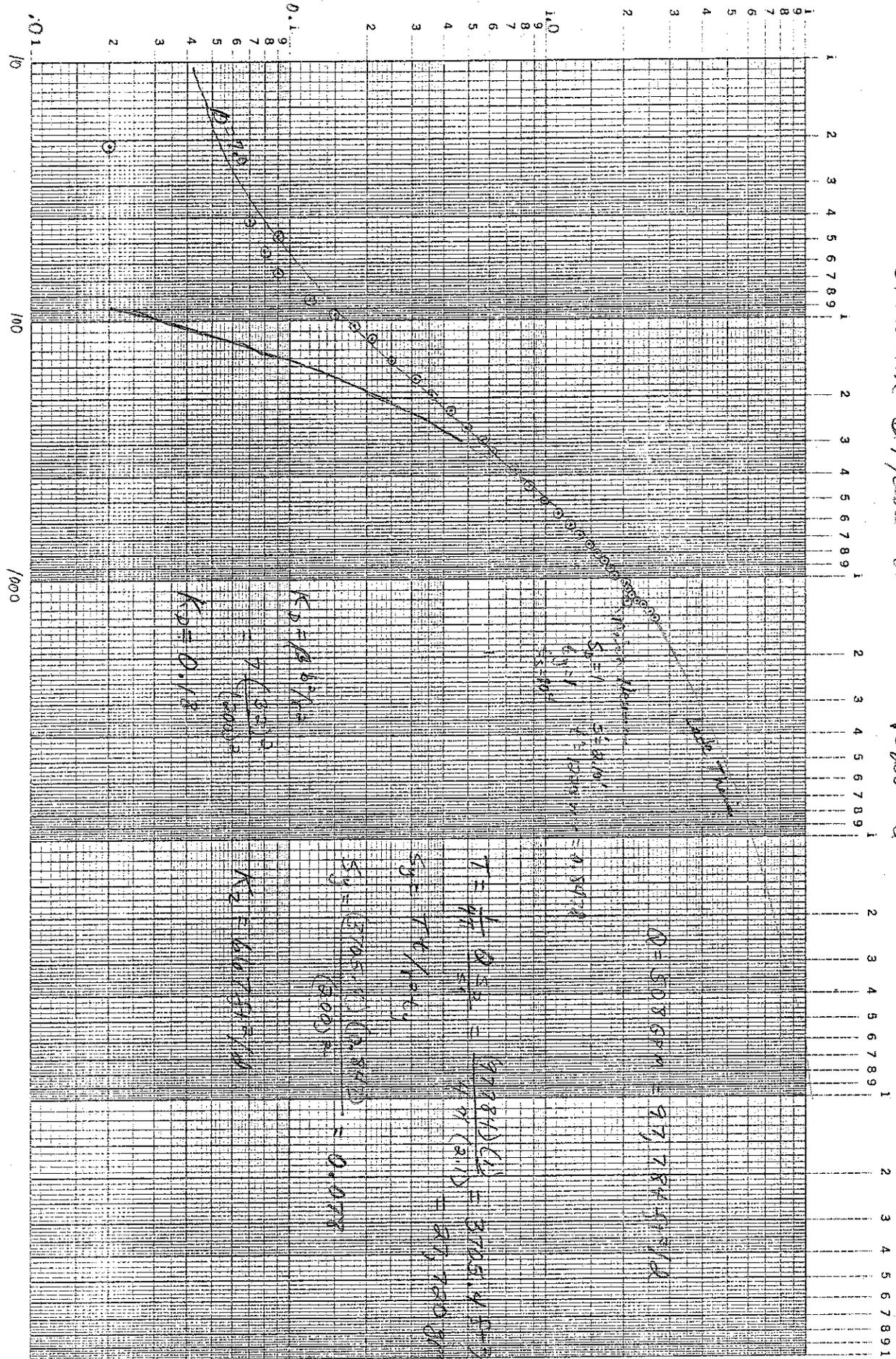
RM#2 - 480 GPM and 320 AF/yr for Irr. of 80 acres

DM#2 - 120 GPM and 80 AF/yr for Irr. of 20 acres

If the total amounts were applied uniformly throughout the irrigation season (April 1 to October 1 or 180 days), the instantaneous withdrawals from RM#2 would average 400 gpm and from DM#2 100 gpm. At the end of the irrigation season, the drawdown resulting from pumping of RM#2 would be about 27 ft at RM#2 and 11 ft at DM#2; pumping at DM#2 would result in a drawdown of 7 ft. at DM#2 and 3 ft. at RM#2. Total drawdown would be 30 ft. at RM#2 and 18 ft. at DM#2. Reportedly there is about 30 ft. of water above the pump intake in RM#2; the above withdrawals are the upper limits under present conditions. Pumping of the DM#2 well at 800 GPM as applied for is not feasible.

D. Martin 34/26E-281

b = 32' sat. thickness  
w = 200' Q = 508 GPM



$$Q = 508 \text{ GPM} = 27,784.5 \text{ gal/d}$$

$$S_D = 1 \quad S = 0.10'$$

$$T = \frac{1}{4\pi} \frac{Q S_D}{r^2} = \frac{(27,784.5)(0.10)}{4\pi (3.15)^2} = 3705.4 \text{ ft}^2/\text{d}$$

$$S_D = T b / 1000$$

$$S_D = \frac{(3705.4)(10)}{(3000)^2} = 0.0478$$

$$K_D = \frac{7(1.5-1.3)}{12000}$$

$$K_D = 6.167 \times 10^{-5} \text{ /ft}$$

$$K_D = 0.13$$

T (minutes)

$$400 \text{ AF} \times 3.25 \times 10^5 = 1.30 \times 10^8 \text{ GALLONS}$$

$$600 \text{ AF} \times \quad \quad \quad = 1.96 \times 10^8 \text{ GALLONS}$$

IF PUMP 600 GPM CONTINUOUSLY - 150 DAYS TO PUMP 400 AF.

" " 800 GPM " " 170 DAYS TO PUMP 600 AF

AFTER 150 DAYS OF CONTINUOUS PUMPING  
BY R. MARTIN (600 gpm) & D. MARTIN (800 gpm)  
THE D/D'S WOULD BE?

R. MARTIN -  
AT 1' AWAY

$$U = \frac{1.87 \times 1 \times 0.8}{3.3 \times 10^4 \times 150} = 3.02 \times 10^{-8} \quad WU = 16.74 \quad S = \frac{114.6 \times 600 \times 16.74}{3.3 \times 10^4} = 34.88'$$

AT r = 169'

$$U = \frac{1.87 \times 169^2 \times 0.8}{3.3 \times 10^4 \times 150} = 8.63 \times 10^{-4} \quad WU = 6.48 \quad S = 13.50'$$

D. MARTIN -

ONE FOOT FROM WELL

$$U = 3.02 \times 10^{-8} \quad WU = 16.74 \quad S = \frac{114.6 \times 800 \times 16.74}{3.3 \times 10^4} = 46.51'$$

169 FEET FROM WELL

$$U = 8.63 \times 10^{-4} \quad WU = 6.48 \quad S = 13'$$

D/D AT R. MARTIN'S WELL 53' & D/D AT D. MARTIN'S WELL 60'

D. MARTIN HAS 30' OF WATER IN WELL (73' TO 103')  
R MARTIN HAS 30' " " " " (73' TO ?) ASSUME

ie.  $s = 30'$   $Q = 400 \text{ gpm}$  FROM R.M.'S & D.M.'S WELLS  
$$U(u) = \frac{s \cdot T}{14.6 \times Q} = \frac{15 \times 3.3 \times 10^4}{14.6 \times 400} = 10.80 \quad U = 2.34 \times 10^{-10}$$

$$t_{\text{days}} = \frac{1.87 r^2 S}{T U}$$

1 FOOT FROM PUMPED WELL

$$t_{\text{days}} = \frac{1.87 \times 1 \times 0.8}{3.3 \times 10^4 \times 2.34 \times 10^{-10}} = \frac{1.87 \times 8 \times 10^{-2} \times 10^6}{3.3 \times 2.34} = 19373 \text{ Days}$$

168 FEET FROM PUMPED WELL

R.M. HAS ONLY 80 AC OF 100 AC - IRR. NEEDS

$$\frac{80}{100} \times 600 = 480 \text{ gpm} \rightarrow 320 \text{ AF/YR}$$

$$\text{D.M. HAS RIGHT TO } \frac{20}{100} \times 600 = 120 \text{ gpm} \rightarrow 80 \text{ AF/YR}$$

IRR SEASON APR. 1 TO OCT. 1

IF R.M. IRR CONTINUOUSLY AT 480 gpm  
AND PUMPS ~~NEEDS~~ 320 AF/YR ( $= 1.04 \times 10^8 \text{ G}$ )  
IN 151 DAYS

DRAWDOWN 1' FROM R MARTIN:

$$U = \frac{1.87 \times 1 \times .08}{3.3 \times 10^4 \times 151} = 3.00 \times 10^{-8} \quad WU = 16.7449$$

$$S_1 = \frac{114.6 \times 480 \times 16.75}{3.3 \times 10^4} = 27.92'$$

D/D 169' FROM PUMPED WELL

$$U = \frac{1.87 \cdot 169^2 \cdot .08}{3.3 \times 10^4 \cdot 151} = 8.57 \times 10^{-4} \quad WU = 6.48$$

$$S_{169} = \frac{114.6 \times 480 \times 6.48}{3.3 \times 10^4} = 10.80'$$

IF D. MARTIN PUMPS SIMULTANEOUSLY AT 120 gpm HE WILL HAVE W/DRAWN 80 AF IN 151 DAYS

D/D 1' FROM DM WELL

$$U = 3.00 \times 10^{-8} \quad WU = 16.7449$$

$$S_1 = \frac{114.6 \times 120 \times 16.75}{3.3 \times 10^4} = 6.98'$$

D/D 169' FROM DM WELL

$$U = 8.57 \times 10^{-4} \quad WU = 6.48$$

$$S_{169} = \frac{114.6 \times 120 \times 6.48}{3.3 \times 10^4} = 2.7'$$

~~T/D R.M. WELL~~ w/ R.M. w/DRAWING 480 GPM CONTINUOUSLY FOR 151 DAYS & T.M. w/DRAWING 120 GPM FOR 151 DAYS:

R.M. well  $27.9' + 2.7' = 30.6'$

D.M. "  $7.0' + 10.8' = 17.8'$

IF RM & DM EXTEND PUMPAGE THROUGHOUT IRR SEASON (APR 1 - OCT 1) OR 180 DAYS?

Q<sub>RM</sub> = 400 gpm x 180 DAYS = 320 AF/YR

DD 1 FT FROM RM WELL: U = (1.87 x 10<sup>0.7</sup> x 10<sup>8</sup>) / (3.3 x 10<sup>4</sup> x 180) = 2.5 x 10<sup>-3</sup> w<sub>u</sub> = 16.93

S<sub>i</sub> = (114.6 x 400 x 16.93) / (3.3 x 10<sup>4</sup> x 2.9 x 10<sup>4</sup>) = 23.52' ←

DD 16 FT FROM RM WELL: U = (1.87 x 16<sup>2</sup> x 10<sup>8</sup>) / (3.3 x 10<sup>4</sup> x 180) = 7.2 x 10<sup>-4</sup> w<sub>u</sub> = 6.66

S<sub>16ft</sub> = (114.6 x 400 x 6.66) / (3.3 x 10<sup>4</sup> x 2.9 x 10<sup>4</sup>) = 9.25' ←

Q<sub>DM</sub> = 100 gpm (x 180 DAYS = 80 AF/YR)

DD 1 FT FROM DM WELL: U = 2.5 x 10<sup>-3</sup> w<sub>u</sub> = 16.93

S<sub>i</sub> = (114.6 x 100 x 16.93) / (3.3 x 10<sup>4</sup> x 2.9 x 10<sup>4</sup>) = 6.69', 5.38' ←

DD 16 FT FROM DM WELL: U = 7.2 x 10<sup>-4</sup> w<sub>u</sub> = 6.66

S<sub>16ft</sub> = 2.63', 2.31' ←

DD AT RM WELL - 26.8 + 2.6 = 29.4'
" " DM " " 6.7' + 10.5' = 17.2'

6/7

MAINTAIN RM WELL AT 400 GPM & 180 DAYS  
OF CONTINUOUS PUMPING

ALLOW D/D AT RM WELL TO REACH <sup>30</sup> 25 FEET. WHAT  
CAN DM PUMP OVER 180 DAY INTERVAL?

$S_{RM} = \frac{30'}{25'}$  WL IN RM WELL IS DRAWN DOWN  
26'  
17' i.e. INCREASED PUMPAGE BY DM CAN REDUCE  
WL IN RM WELL BY  $30 - 26 = 4'$

$$S_{DM} = 4' = \frac{114.6 Q W U}{T} = Q = \frac{4 \times 3.3 \times 10^4}{114.6 \times 6.66} = 173 \text{ GPM}$$

$$S_{DM} = \frac{114.6 \times 173 \times 16.93}{3.3 \times 10^4} = 10.17$$

D/D AT DM WELL PUMPING AT 173 GPM  
AND RM " " " 400 GPM

$$\Rightarrow 10.17 + 9.25 \approx 30'$$

PLACEMENT OF THREE WELLS PUMPING AT 550 GPM  
FOR 180 DAYS. WHAT IS  $s$  AT  $r=1$ ?

$$U = \frac{187 \times 1 \times .08}{3.3 \times 10^4 \times 180} = 2.51 \times 10^{-8} \quad W(u) = 16.9$$

$$s = 32.38'$$

$$r = ? \quad \text{AT } s = 1'$$

$$W(u) = \frac{3 \times T}{114.6 Q} = 0.52$$

$$U = 5.3 \times 10^{-1}$$

$$r = \left( \frac{U T t}{187 \times s} \right)^{1/2} = 4587'$$

AQUIFER TEST

R MARTIN & G. MARTIN WELLS

DATE, 1977

CALCULATIONS

$$U = \frac{1.87 \times r^2 S}{T t_{\text{days}}}$$

$$S = \frac{114.6 Q \times W U}{T}$$

$$T = \left( \frac{3.7 + 2.9}{2} \right) 10^4 = 3.3 \times 10^4 \text{ gpd/ft}$$

$$S = \frac{.07}{.08}$$

$$r = 169 \text{ ft}$$

$$U = \frac{1.87 \times r^2 \cdot .08}{3.3 \times 10^4 t_{\text{days}}}$$

$$S = \frac{114.6 Q \times W U}{3.3 \times 10^4}$$

R MARTIN	600 gpm	400 AF/YR
D. MARTIN	800 gpm	600 AF/YR

1 FOOT FROM  
PUMPED WELL

$$U = \frac{1.87 \times 1 \times .08}{3.3 \times 10^4 t_{\text{day}}} = \frac{4.53 \times 10^{-6}}{t_{\text{day}}} \quad 11.7336$$

1 DAY

$$W U = 11.7336$$

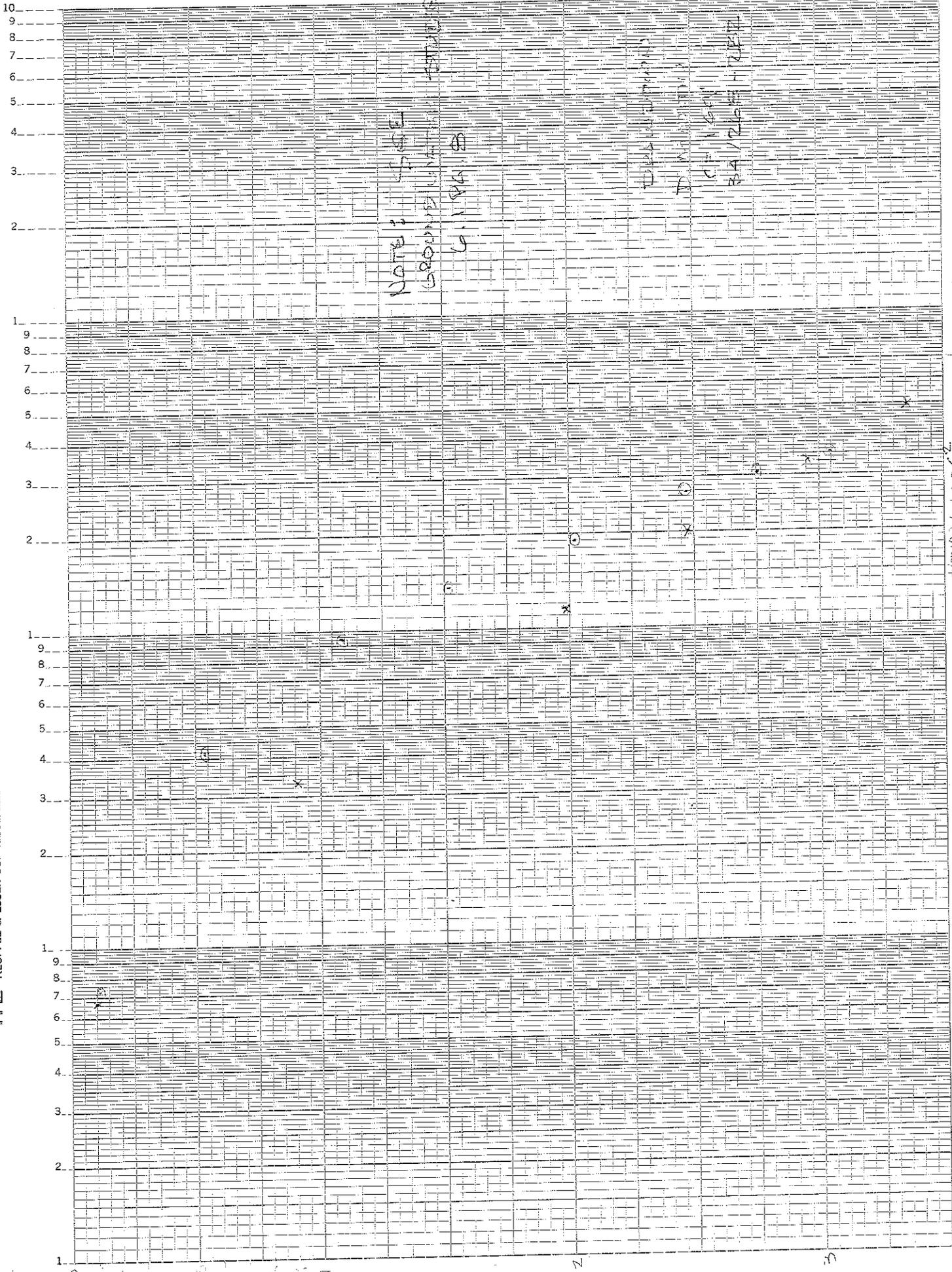
$$S (\text{ft/day}) = \frac{114.6 \times 600 \times 11.7336}{3.3 \times 10^4} = 24.45 \text{ FT}$$

D/D AT D MARTIN'S WELL (r=169') t<sub>day</sub>=1

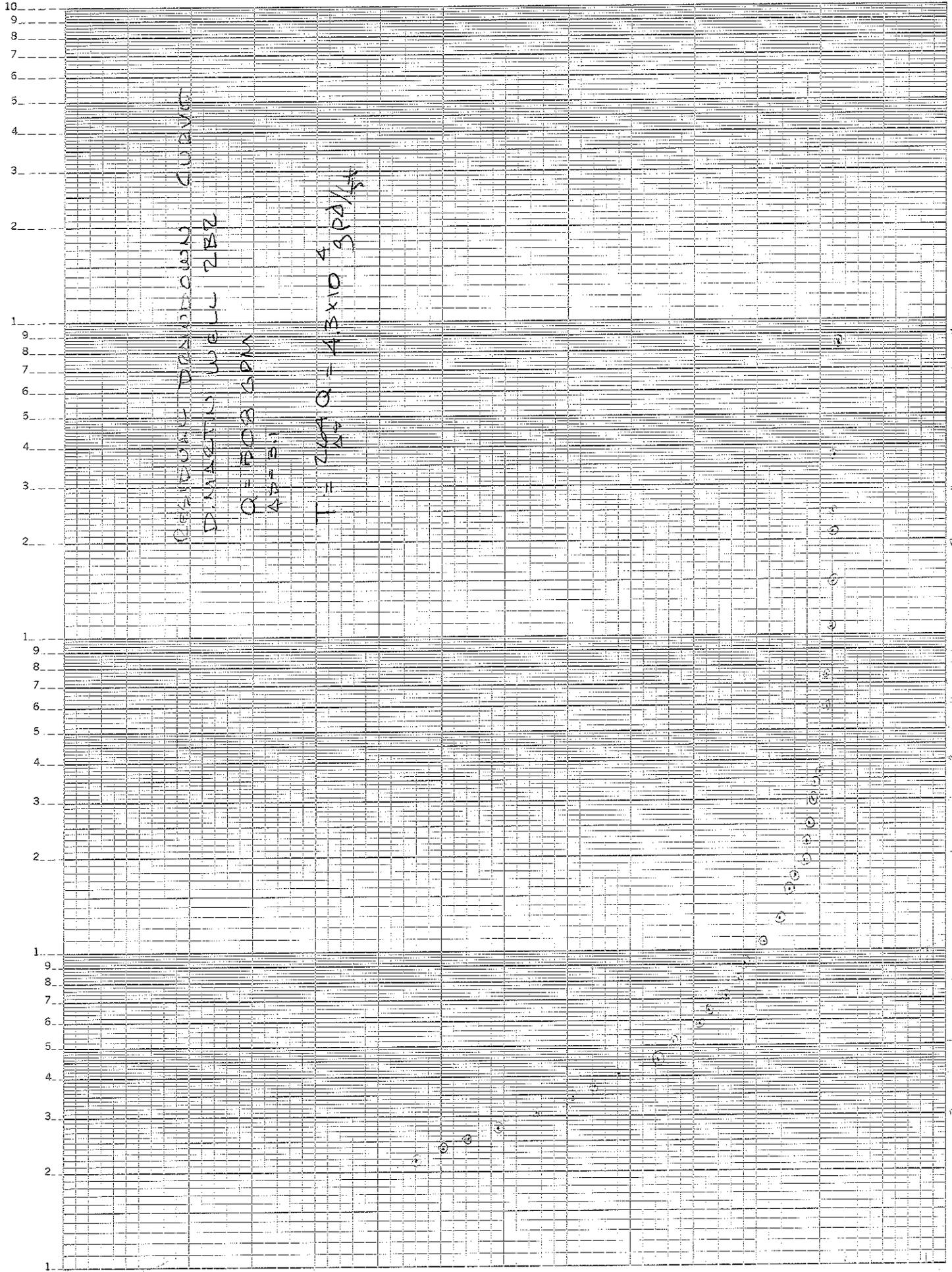
$$U = \frac{1.87 \times 169^2 \times .08}{3.3 \times 10^4} \cdot .13 \Rightarrow \frac{114.6 \times 600 \times 1.5889}{3.3 \times 10^4} = 3.31 \text{ FT}$$

46 6010

SEMI-LOGARITHMIC 4 CYCLES X 70 DIVISIONS  
KEUFFEL & ESSER CO. MADE IN U.S.A.



$\Xi$	$\pm/1440 r^2$	$w(\omega)$	$1/\omega$
2.11	$7.29 \cdot 10^{-7}$	1.500	67
2.55	$3.51 \cdot 10^{-5}$	.91	3.33
2.76	$3. \cdot 10^{-5}$	1.97	11.76
2.48	2.68 "	2.47	26.0
2.02	1.95 "	2.96	33.3
1.52	1.37 "	3.35	50.0
1.09	$9.36 \cdot 10^{-6}$		
.53	$4.13 \cdot 10^{-6}$		



1000  
100  
10  
1



AQUIFER TEST

Owner R. MARTIN Location 3A/26E-2C2 Well No. PUMP  
 Date 10-11-77 Meas. by W.W.M & PG Test PUMP County OK  
 Meas. point 1.1' A.G.L Elev. Meas. Point ALLEGY HOLE BELOW PUMP  
 Meas. equipment E-TAPE  
 DTW 74.52  $t_0$  1140 HRS  $Q$  508 GPM  $r$  0

Date	Hour	Water level			s	t (Min)	1440r <sup>2</sup> t	Remarks
		Held	Wet	Depth (DTW)				
10/11/77	11:40:00	90.5	15.48	74.52	0.0	0.0		
	1:30	105	-2.21	86.79	12.27	1.5		
	2	105	-2.20	87.66	13.14	2.0		
	3:00		-0.81	89.13	14.61	3.0		
	F		-1.67	89.33	14.81	4.0		
	4:30	105	-1.5	90.00	15.48	4.5		
	5:00	105.16	-1.5	90.16	15.64	5.0		
	6:00	105.95	-1.5	90.45	15.93	6.0		
	7:00	105.63		90.63	16.11	7.0		
	11:00	106.72		91.32	16.80	11		
	12:00	106.89		91.48	16.96	12		
	13:00	106.54		91.54	17.02	13		
	14:00	106.64		91.64	17.12	14		
	15	106.76		91.76	17.24	15		
	16	106.84		91.84	17.32	16		
	17:00			92.14	17.62	20		
	18:00	107.19		92.40	17.88	25		
	19:00	107.38		92.38	17.86	30		
	20:00	108.05		93.05	18.53	35	TAPE ONLY	
	21:00	107.62		92.62	18.10	40		
	22:00	110-	-1.12	93.68	19.16	45		
	23:00	110	-1.12	93.88	19.36	50		
	24:00	110	-0.89	94.11	19.59	60	TAPE PROBLEMS	





AQUIFER TEST

Owner R. MARTIN Location 34/26E-7C2 Well No. \_\_\_\_\_  
 Date <sup>(WED)</sup> 10-12-77 Meas. by W.W.M. Test REC County OK.  
 Meas. point 1.1A GL - HOLE IN BASE OF PUMP Elev. Meas. Point \_\_\_\_\_  
 Meas. equipment E. TAPE  
 DTW 74.52 t<sub>0</sub> 1200 HRS Q \_\_\_\_\_ r 0

Date	Hour	Water level			s	t	1440r <sup>2</sup> t	Remarks
		Held	Wet	Depth (DTW)				
10/12/77	1200.5	100	-5	85		5		
		103	27	83.72		1.0		
		105	-2.2	82.27		2.0		
		96.82		81.82		3.0		
		96.40		81.40		4.0		
		96.24		81.24		4.5		
		96.12		81.12		5		
		95.98		80.98		6		
		95.80		80.82		7		
		95.70		80.70		8		
		95.61		80.61		9		
		95.47		80.49		10		
		95.42		80.42		11		
		95.32		80.32		12		
		95.28		80.28		13		
		95.24		80.20		14		
	1215	95.13		80.13		15		
	1220	95.11		80.11		20		
	1225	94.68		79.68		25		
	1230	94.46		79.46		30		
	1235	94.29		79.29		35		
	1240	94.14		79.14		40		
	12	94.02		79.02		45		

17 - 50 - 5  
 30 - 100 - 10  
 100 - 200 - 15  
 200 - 300 - 20  
 300 - 400 - 25  
 400 - 500 - 30  
 500 - 600 - 35  
 600 - 700 - 40  
 700 - 800 - 45  
 800 - 900 - 50  
 900 - 1000 - 55



AQUIFER TEST

Recovery  
Sheet 2 of 3

Owner R. MARTIN Location 3A/26E-2C7 Well No. 1  
 Date 10-12-77 Meas. by WWM, PG, LR Test REC County OK  
 Meas. point 11 AGL Elev. Meas. Point \_\_\_\_\_  
 Meas. equipment E. TP  
 DTW 74.52  $t_0$  12004250  $\frac{60}{2.5 \times 55}$  r 0

Date	Hour	Water level			s	t	1440r <sup>2</sup> t	Remarks
		Held	Wet	Depth (DTW)				
10/12	1250	92.91	-15	78.3		50		
	1300	93.75	-5			60		
	1310	94.03	No	Good		70	LOST WEIGHT NOT CALIB	
	1315	93.46				75	NEW WEIGHT	
	1320	93.38				80		
	1330	93.38				90		
	1341	93.19				101		
	1400	92.95				120		
	1420	92.79				140		
	1500	92.49				180		
	1535	92.32				215		
	1605	92.21	-15	77.21		245		
	1635	92.10				275		
	1705	92.00				305		
	1805	91.86				365		
	1905	91.72		76.72		425		
	2005	91.64		76.72		485		
	2105	91.55		76.55		545		
	2200	91.50		76.50		605		
	2307	91.41		76.41		667		
10/13	0505	91.30		76.30		725		
	0105	91.26		76.26		785		
	0205	91.16		76.16		845		





AQUIFER TEST

Owner D. MARTIN Location 34/265-2B1 Well No. DB6  
(CAPPED)  
Date 10/11/97 Meas. by PG, WWM Test D/D County LK  
Meas. point LOW. EDGE OF SLOTT IN CASING Elev. Meas. Point 1.0 AGL  
Meas. equipment E-TAPE  
DTW 73.76  $t_0$  11.46  $Q$  508 GPM  $r$  200'

Date	Hour	Water level		Depth (DTW)	s	t	1440r <sup>2</sup> t	Remarks
		Held	Wet					
10/11/97	1140	75.16	-1.40	73.76	0	0		THIS IS ORIG. WELL TAPE IS 1.40' SHORT
			"	"	0	7 MIN.		Q:
			"	73.78	.02	21		55 GAL IN 6.5 SEC
	1221				.07	41 MIN		= 508 GPM
					.09	47		
		75.24		73.84	.08	54		
	1246	75.25			.04	66		
		75.28		73.88	.12	83		
		75.31			.15	95		
		75.34			.18	104		
		75.37			.21	119		
	1402	75.41			.25	142		
	1430	75.47			.31	170		
	1454	75.52			.36	194		
	1524	75.54			.43	224		
	1558	75.65			.49	258		
	1632	75.73			.57	292		
	1705	75.78			.62	325		
	1800	75.92		74.52	.76	380		
	1900	76.03			.87	440		
	2000	76.15			.99	500		
	2100	76.28			1.12	560		
	2200	76.40			1.24	620		





AQUIFER TEST

Owner D. MARTIN Location 34/26E-2B Well No. DBS 1 (CAPPED)  
 Date 10-12-77 Meas. by PG, WWM, LR Test REL. County OK.  
 Meas. point LOW EDGE OF SLOT IN CASING Elev. Meas. Point 1.0' AGL  
 Meas. equipment E-TAPE  
 DTW 73.76  $t_0$  0  $r$  200'

Date	Hour	Water level			s	t	$\frac{1440r^2}{t}$	Remarks
		Held	Wet	Depth (DTW)				
10-12-77	1200	77.78	1.4	76.38	0	0	PUMP OFF	
		77.86			-	50	t = TIME SINCE	
		77.85			-	65	PUMP OFF	
		77.86			-	75		
		77.85			-	85		
		77.83			-	95		
		77.85			-	120		
		77.84			-	150		
		77.77			.01	185		
		77.74			.04	210		
	1400	77.71			.07	240		
	1627	77.67				267		
	1657	77.63				297		
	1800	77.56				360		
	1900	77.48				420		
	2000	77.36				480		
	2100	77.31				540		
	2200	77.22				600		
	2300	77.19				660		
	2400	77.07				720		
	0100	77.00				780		
	0200	76.93				840		
	0300	76.89						





AQUIFER TEST

Owner D. MARTIN Location 34/26E-2B2 Well No. 2 (W/PUMP) <sup>OBS.</sup>  
E OF GRESSUAC. RD.  
 Date 10/11/77 Meas. by PG Test D/D County OK.  
 Meas. point LOWER EDGE OF SLOT IN LSL. Elev. Meas. Point 2.1 AGL  
 Meas. equipment E. TAPE (FISHER M-SLOPE)  
 DTW 75.38'  $t_0$  1140425 @ 508 GPM  $r$  169'

Date	Hour	Water level			s	t	1440r <sup>2</sup> t	Remarks
		Held	Wet	Depth (DTW)				
10/11/77	1140	76.38	-1.0	75.38	0	0	0	TAPE IS 1.0 SHORT
					0	5	8.73x10 <sup>7</sup>	Q: 55 GALLONS
					0	1.0	4.11x10 <sup>7</sup>	IN 6.5 SEC.
					0	1.5	2.7x10 <sup>7</sup>	
					UP 0.01	3.5	1.18x10 <sup>7</sup>	
					0	5.0	8.23x10 <sup>6</sup>	
				75.40	+0.02	9.5	4.33x10 <sup>6</sup>	
				75.42	.04	11.0	3.74x10 <sup>6</sup>	
					.05	13.0	3.16x10 <sup>6</sup>	
	1155			75.435	.055	15.0	2.74x10 <sup>6</sup>	
					.06	17.0	2.42x10 <sup>6</sup>	
					.07	20.0	2.06x10 <sup>6</sup>	
					.09	25.0	1.65x10 <sup>6</sup>	
					.11	30.0	1.37x10 <sup>6</sup>	
					.13	35.0	1.18x10 <sup>6</sup>	
					.145	40.0	1.03x10 <sup>6</sup>	
					.16	45.0	9.14x10 <sup>5</sup>	
	1230				.185	50.0	8.23 "	
					.21	60.	6.85 "	
	1250				.24	70	5.88 "	
	1300				.28	80	5.14 "	
					.31	90	4.57 "	
	1320				.34	100	4.11 "	



AQUIFER TEST

Draw Down

Sheet 2 of 3

Owner D. MARTIN Location 34/26E-2B2 Well No. 2(w/PUMP) <sup>OBS.</sup>  
 Date 10-11-77 Meas. by 76 WWM, LR Test D/D County OK  
 Meas. point LOWER EDGE OF SLOT IN CASING Elev. Meas. Point 2.1 AGL  
 Meas. equipment E-TAPE  
 DTW 75.38  $t_0$  1140 (10-11-77)  $Q$  50 GPM  $r$  169

Date	Hour	Water level			s	t	$\frac{1440r^2}{t}$	Remarks
		Held	Wet	Depth (DTW)				
10-11-77	1330	76.75			.37	110	$3.74 \times 10^5$	
	1405				.47	145	2.84 "	
	1430	76.91			.53	170	2.42 "	
	1500				.61	200	2.06 "	
	1528				.67	228	1.80 "	
	1600	77.14			.76	260	1.58 "	
	1635				.86	295	1.39 "	
	1707				.94	327	1.26 "	
	1805				1.09	385	1.07 "	
	1900				1.21	440	$9.35 \times 10^4$	
	2004				1.43	504	8.16 "	
	2105				1.52	565	7.28 "	
	2203				1.64	623	6.60 "	
	2304				1.83	688	5.98 "	
10-12-77	0004				1.88	744	5.53 "	
	0103				2.02	803	5.12 "	
	0203				2.09	863	4.77 "	
	0303				2.22	923	4.46 "	
	0404				2.32	984	4.18 "	
	0505				2.38	1045	3.94 "	
	0604				2.48	1104	3.73 "	
	0703				2.58	1163	3.54 "	
	0803				2.69	1223	3.36 "	





AQUIFER TEST

Owner D. MARTIN Location 34/26E ZB2 Well No. 2 <sup>OBS. 2</sup> (W/PUMP)

Date 10-12-77 Meas. by TG Test ZEL. County OK.

Meas. point ACCESS SLOT-LOW EDGE Elev. Meas. Point 2.1' AGL

Meas. equipment FISHER M-SLOPE

DTW 75.38  $t_0$  0  $r$  169'

Date	Hour	Water level		Depth (DTW)	RESIDUAL DRAIN DOWN	t'	$\frac{1440r^2}{t'}$	Remarks
		Held	Wet					
10-12-77	1200	80.00 - .55	78.45	78.45	3.07	0	-	PUMP OFF
		.54		78.46	3.08	2.0	731	(PUMP HAD BEEN ON 1460 MIN.)
		.56		78.44	3.06	4.0	366	t = time (min) since pump on.
		.57		78.43	3.05	6.0	244	t' = time (min) since pump off.
		"	"	"	"	7.0	210	
		"	"	"	"	10.0	147	
		.58		78.42	3.04	14.0	105	
		.59		78.41	3.03	20.0	74	
		.59		"	"	25.0	59	Pulled TAPE -
		.62		78.38	3.00	42.0	36	only
		.64		78.36	2.98	45.0	33	
		.65		78.35	2.97	50.0	30	
		.66		78.34	2.96	62.0	25	
		.67		78.33	2.95	70.0	22	
		.68		78.32	2.94	80.0	19	
		.72		78.28	2.90	90.0	17.2	
	1340	.74		78.26	2.88	100.0	15.6	
		.78		78.22	2.84	125.0	12.7	
		.84		78.16	2.78	153.0	10.5	
		.91		78.09	2.71	183.0	8.98	
	1530	.94		78.06	2.68	210.0	7.95	
		.99		78.01	2.63	240.0	7.08	
	1630	1.06		77.94	2.56	270	6.41	



AQUIFER TEST

RECOVERED  
 Sheet 2 of 2

Owner D. MARTIN Location 34/26E-2B2 Well No. 2 <sup>OBS</sup> (w/pump)  
 Date 10-12-77 Meas. by PG, WWM, LR Test REC County OK  
 Meas. point ACCESS SLOT-LOW EDGE Elev. Meas. Point. 2.1' AGL  
 Meas. equipment E-TAPE  
 DTW 75.38 t<sub>0</sub> 0 t<sub>1</sub> 169

Date	Hour	Water level			READ DTW	t'	1440r2 t/E	Remarks
		Held	Wet	Depth (DTW)				
10-12-77	1700	<del>80.00</del> 71.10	78.90	77.90	2.52	300	5.87	TAPE IS 1.6 SALES
	1800	1.20	78.80	77.80	2.42	360	5.06	
	1900				2.36	420	4.48	
	2000				2.20	480	4.04	
	2103				2.11	543	3.69	
	2200				2.02	600	3.43	
	2300				2.00	660	3.21	
	2400				1.88	720	3.03	
10-13-77	0100				1.92	780	2.87	
	0200				1.73	840	2.74	
	0305				1.67	905	2.61	
	0403				1.61	963	2.52	
	0505				1.55	1025	2.42	
	0605				1.51	1085	2.35	
	0703				1.44	1143	2.28	
	0803				1.42	1203	2.21	
	0840				1.40	1240	2.18	1.40 BELOW SWL AT BEGINNING OF TEST



10/11/77

Leo

~~1/2~~

55 gals 6" main line



10-11-77

- |                            |                            |
|----------------------------|----------------------------|
| 1- 11 41 AM - 6 sec        | 24-12 27 PM - 6 1/2 sec    |
| 2- 11 44 " - 6 1/2 sec     | 25-12 29 PM - <u>7</u> sec |
| 3- 11 46 AM - 6 1/2 sec    | 26-12 31 PM - 6 1/2 sec    |
| 4- 11 48 AM - 6 1/2 sec    | 27-12 33 PM - 6 1/2 sec    |
| 5- 11 50 AM - 6 1/2 sec    | 28-12 35 PM - 6 1/2 sec    |
| 6- 11 52 AM - 6 1/2 sec    | 29-12 37 PM - <u>7</u> sec |
| 7- 11 54 AM - 6 1/2 sec    | 30-12 39 PM - 6 1/2 sec    |
| 8- 11 56 AM - 6 1/2 sec    | 31-12 41 PM - 6 1/2 sec    |
| 9- 11 58 AM - 6 1/2 sec    | 32-12 43 PM - <u>7</u> sec |
| 10-12 00 PM - 6 1/2 sec    | 33-12 45 PM - 6 1/2 sec    |
| 11-12 01 PM - <u>7</u> sec | 34-12 47 PM - 6 1/2 sec    |
| 12-12 03 PM - 6 1/2 sec    | 35-1 00 PM - 6 1/2 sec     |
| 13-12 05 PM - 6 1/2 sec    | 36-1 05 PM - 6 1/2 sec     |
| 14-12 07 PM - 6 1/2 sec    | 37-1 25 PM - 6 1/2 sec     |
| 15-12 09 PM - <u>7</u> sec | 38-1 40 PM - 6 1/2 sec     |
| 16-12 11 PM - 6 1/2 sec    | 39-1 47 PM - <u>7</u> sec  |
| 17-12 13 PM - <u>7</u> sec | 40-1 50 PM - 6 1/2 sec     |
| 18-12 15 PM - 6 1/2 sec    | 41-1 53 PM - 6 1/2 sec     |
| 19-12 17 PM - 6 1/2 sec    | 42-1 35 - 6 1/2 "          |
| 20-12 19 PM - 6 1/2 sec    | 43-1 520 - 6 1/2 "         |
| 21-12 21 PM - <u>7</u> sec | 44-1 620 - 6 1/2 "         |
| 22-12 23 PM - 6 1/2 sec    | 45- 1 715 - 6 1/2 "        |
| 23-12 25 PM - 6 1/2 sec    | 46- 1 915 - <u>7</u> "     |

47 215 7.5sec

48 2210 6.55sec

49 0010 7.05sec 10-12-77

50 0212 6.85sec

51 0403 6.55sec

52 0609 - 6.55sec

53-0709 - 6.55sec

54-0803 - 6.55sec

55-1125-6.55sec 10 12 77

Leo

AQUIFER TEST  
MARTIN WELLS, OKANOGAN COUNTY, WASHINGTON

At the request of personnel of the Central Region, an aquifer test was conducted on October 11, 12, 13, 1977 near Omak in Okanogan County.

The primary purpose of the test was to determine possible hydraulic continuity between the wells, and aquifer constants.

Three wells were used in the test. The pumped well (RM #2) belongs to Mr. R. Martin and is located in 34/26E-2C2. The two wells which were used for observational purposes are owned by Mr. D. Martin and are 34/26E-2B2 (DM #2) which is 169 feet ESE of the pumped well and 34/26E-2B1 (DM #1) which is 31 feet east of DM#2 and 200 feet ESE of RM#2 (Figure 1).

The wells are developed in an unconfined aquifer of Quaternary age consisting of clasts ranging in size from silt to boulders which were deposited by glacial melt water streams. Outcrops of bedrock throughout the immediate area constitute impermeable boundary conditions which complicate the interpretation of the test data. No significant pumping had taken place for several days before the test and the aquifer was assumed to be essentially in a nonstressed condition.

The electric turbine pump was started at 1140 hrs. on October 11, 1977 and a pumping rate (Q) of 508 gallons per minute (gpm) was quickly established and maintained. Q, determined by timing the filling of a 55 gallon container, was checked repeatedly throughout the 24 hour pumping test. Drawdown measurements were made in all three wells; however, because of difficulties encountered

in getting reliable readings none were taken in the pumped well during the last 18 hours of pumping.

After 24 hours, the water levels in DM#2 and DM#1 had dropped 3.05 feet and 2.63 feet respectively. The pump was shut off and recovery was measured. After 10 hours, wells DM#2 and DM#1 had recovered to within 1.40 ft. and 1.44 ft., respectively, of the static water levels measured at the beginning of the test. The pumped well (RM#2) had recovered to within 1.33 ft. of the prepumping level. Copies of all data are attached.

The drawdown data for the observation well DM#2 were plotted on logarithmic graph paper (Fig. 2) and using the curve corresponding to the latter part of the test and the Theis type curve, a transmissivity (T) of  $2.9 \times 10^4$  gallons per day per foot (gpd/ft) and a storage coefficient (S) of .07 were determined.

Using the following formulae and constants, one can investigate withdrawal/drawdown possibilities. It is stressed that the calculated figures are probably conservative because of the likelihood of additional impermeable boundaries.

$$U = \frac{1.87 \times r^2 \times S}{T \times t \text{ days}} \quad s = \frac{114.6 \times Q \times W_u}{T}$$
$$T = 2.9 \times 10^4 \text{ gpd/ft} \quad S = .07$$
$$r = 169 \text{ ft (distance from RM\#1 to DM\#2)}$$

A groundwater certificate for 600 gpm and 400 AF/yr for the irrigation of 100 acres from RM#1 has been issued. Of the 100 acres, 80 acres is for land belonging to Ralph Martin and 20 acres is for land owned by Dean Martin.

If the place of withdrawal for the irrigation of 20 acres were changed to DM#2, the following would apply:

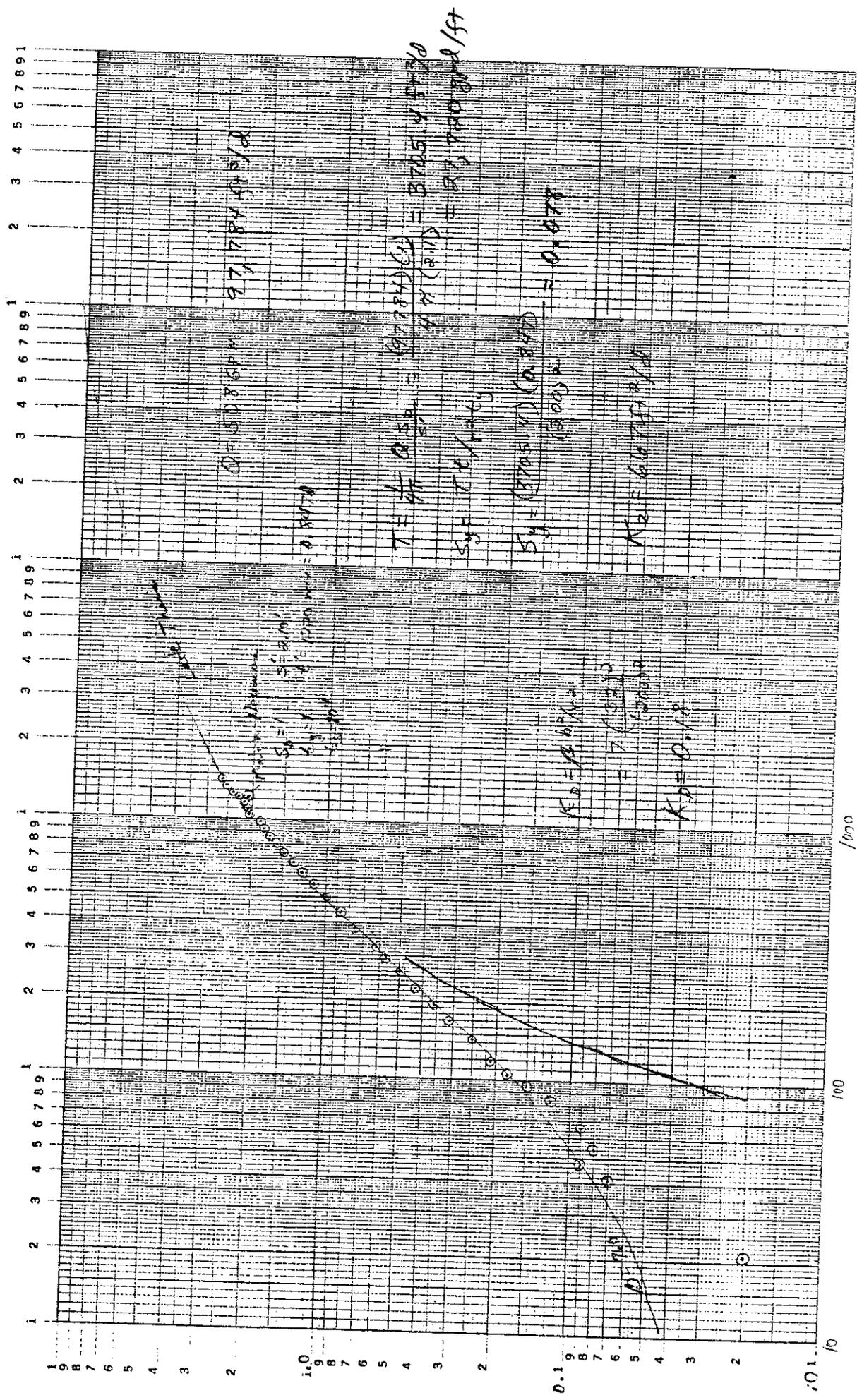
RM#2 - 480 GPM and 320 AF/yr for Irr. of 80 acres

DM#2 - 120 GPM and 80 AF/yr for Irr. of 20 acres

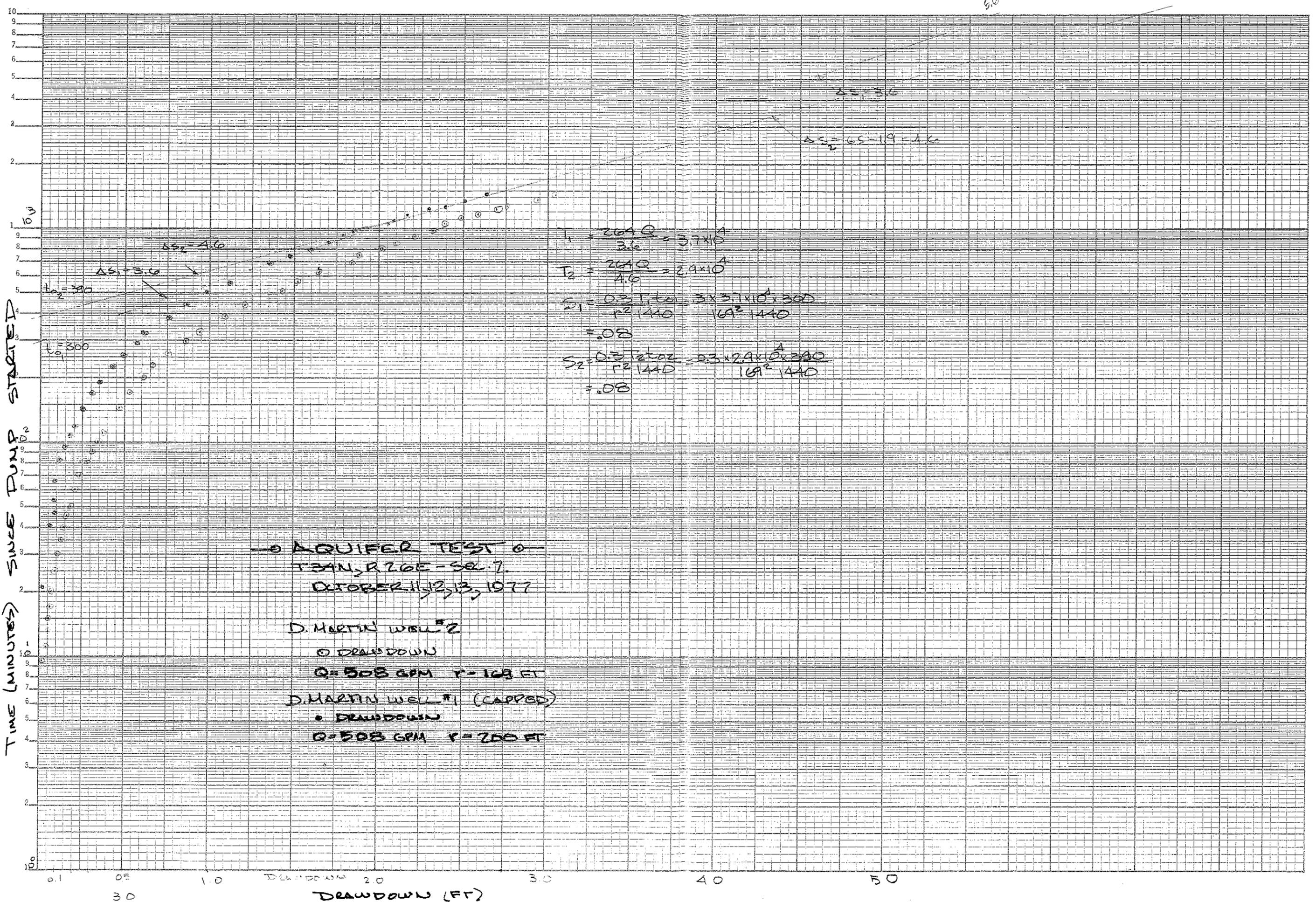
If the total amounts were applied uniformly throughout the irrigation season (April 1 to October 1 or 180 days), the instantaneous withdrawals from RM#2 would average 400 gpm and from DM#2 100 gpm. At the end of the irrigation season, the drawdown resulting from pumping of RM#2 would be about 27 ft at RM#2 and 11 ft at DM#2; pumping at DM#2 would result in a drawdown of 7 ft. at DM#2 and 3 ft. at RM#2. Total drawdown would be 30 ft. at RM#2 and 18 ft. at DM#2. Reportedly there is about 30 ft. of water above the pump intake in RM#2; the above withdrawals are the upper limits under present conditions. Pumping of the DM#2 well at 800 GPM as applied for is not feasible.

b = 38' sat. thickness  
 v = 200' Q = 508 GPM

D. Martin B4/26E - 2E1



T (minutes)



○ AQUIFER TEST ○  
T34N, R26E - S27  
OCTOBER 11, 12, 13, 1977

D. MARTIN WELL #2  
○ DRAWDOWN  
Q = 508 GPM r = 168 FT

D. MARTIN WELL #1 (CAPPED)  
○ DRAWDOWN  
Q = 508 GPM r = 200 FT

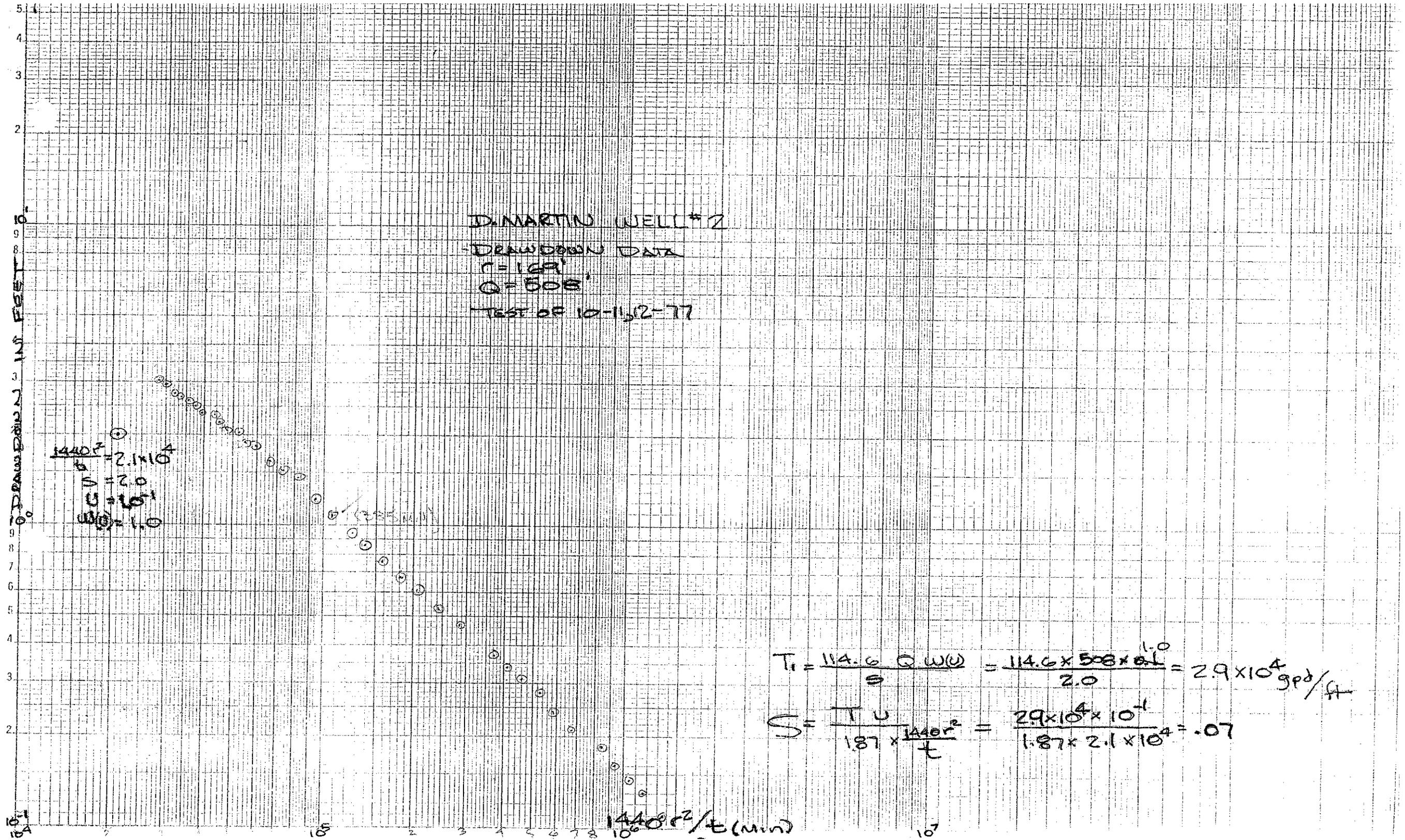
$$T_1 = \frac{204Q}{3.6} = 3.7 \times 10^4$$

$$T_2 = \frac{264Q}{4.6} = 2.9 \times 10^4$$

$$S_1 = \frac{0.3T_1/t_{01}}{r^2/1440} = \frac{3 \times 3.7 \times 10^4 \times 390}{168^2 \times 1440} = 0.08$$

$$S_2 = \frac{0.3T_2/t_{02}}{r^2/1440} = \frac{0.3 \times 2.9 \times 10^4 \times 300}{168^2 \times 1440} = 0.08$$

5.6



D. MARTIN WELL #2  
 DRAWDOWN DATA  
 r = 189'  
 Q = 508'  
 TEST OF 10-11-2-77

1440r<sup>2</sup>/  
 t = 2.1 x 10<sup>4</sup>  
 S = 2.0  
 U = 10<sup>-1</sup>

$$T_r = \frac{114.6 Q W(u)}{S} = \frac{114.6 \times 508 \times 1.0}{2.0} = 2.9 \times 10^4 \text{ gpd/ft}$$

$$S = \frac{T U}{1.87 \times \frac{1440r^2}{t}} = \frac{2.9 \times 10^4 \times 10^{-1}}{1.87 \times 2.1 \times 10^4} = .07$$

1440r<sup>2</sup>/  
 t (min)